

# INDIAN MARITIME UNIVERSITY

(A Central University, Government of India)

## M. Tech. (Marine Engineering & Management)

May-June 2018 End Semester Examinations

SEMESTER-II

### Cryogenic and LNG Vessels (PG13E1201)

Date: 04-06-2018

Time: 3 Hrs

Maximum Marks: 100

Pass Marks: 50

**Note:** Answer any five questions. Assume any missing data.

All questions carry equal marks.

(5×20=100 Marks)

1. Explain the operation of Simple Linde-Hampson Process with a schematic diagram and T-S diagram for liquefaction process.
2. Find the fraction of liquefaction ( $y$ ), the work of liquefaction ( $W_l$ ) and the Figure of Merit (FOM) for 200 atm pressure delivered by the compressor in a Pre-cooled Linde-Hampson cycle operating with nitrogen. The inlet stream is at 1 atm and 300 K. Liquid nitrogen is removed at 1 atm. Freon-12 is used as the refrigerant for pre cooling. The ratio of mass of refrigerant used to the total mass of gas compressed,  $r = 0.1$ . Assume a 5 K temperature difference at approach for the heat exchanger. Enthalpy data for the refrigerant:  $h_a = 207.94$  J/g,  $h_b = 250.2$  J/g,  $h_c = 61.23$  J/g.

Required entropy and enthalpy data (from T-s diagram for nitrogen) are as follows:

Stream	Pressure (atm)	Temperature (K)	Enthalpy (J/g)	Entropy (J/g-K)
1	1	300	462	4.42
2	200	300	430	2.75
6	1	77	35	0.5
9	1	295	457	

3. What is the advantage of NTU-effectiveness approach over LMTD method in case of design of heat exchanger. Derive the expression of NTU-effectiveness relationship for counterflow heat exchanger.
4. In the counterflow heat exchanger in a nitrogen liquefaction system, warm nitrogen gas ( $c_h = 1.600$  kJ/kg-K =  $0.382$  Btu/lbm- $^{\circ}$ R) enters at  $100$  K and  $1$  atm. Cold nitrogen gas ( $c_c = 0.251$  kJ/kg-K =  $0.251$  Btu/lbm- $^{\circ}$ R) enters at  $78$  K ( $140$   $^{\circ}$ R) and  $1$  atm.

(101.3 kPa or 14.7 psia) at a mass flow rate of 0.80 kg/s (6349 lbm/hr). The overall heat transfer coefficient for the heat exchanger is 150 W/m<sup>2</sup>-K (26.4 Btu/hr-ft<sup>2</sup>-°F), and the heat transfer surface area is 50 m<sup>2</sup> (538 ft<sup>2</sup>). Determine the heat transfer rate for the exchanger and the exit temperature of both streams. The ineffectiveness for the counterflow heat exchanger may be determined from following equation:

$$(1 - \varepsilon) = \frac{(1 - C_R) \exp[-N_{tu}(1 - C_R)]}{1 - C_R \exp[-N_{tu}(1 - C_R)]}$$

The terms have their usual meaning.

5. Describe the various modes of two-phase flow in pipe. Explain the application of the Baker diagram in predicting two-phase flow regimes in cryogenic systems.
  
6. Two-phase nitrogen flows in a horizontal 8-in nominal SCH 5 pipe (inside diameter, 8.407 in or 213.5 mm) at a total mass flow rate of 4.50 kg/s (35,700 lbm/hr). The fluid temperature is 85 K (153°R), and the corresponding saturation pressure is 228 kPa (33.1 psia). The quality of the two-phase mixture is 0.150, and the length of the pipe is 800 m (2645 ft). Determine the two-phase frictional pressure drop, assuming that the fluid quality is relatively constant.

The properties of liquid and vapor nitrogen at 85 K and saturation conditions are as follows:

liquid density,  $\rho_L = 771.0 \text{ kg/m}^3 = 48.13 \text{ lbm/ft}^3$

vapour density,  $\rho_G = 9.789 \text{ kg/m}^3 = 0.611 \text{ lbm/ft}^3$

liquid viscosity,  $\mu_L = 0.119 \text{ mPa-s} = 0.119 \text{ cP}$

surface tension,  $\sigma_L = 7.18 \text{ mN/m} = 0.00049 \text{ lbf/ft}$

The viscosity of the vapour phase,

$$\mu_G = 6.21 \text{ } \mu\text{Pa-s}$$

Lockhart-Martinelli parameter,

$$(X_{tt})^2 = \left( \frac{1-x}{x} \right)^{1.8} \left( \frac{\mu_L}{\mu_G} \right)^{0.2} \left( \frac{\rho_G}{\rho_L} \right)$$

Lockhart -Martinelli Correlation

$$\Delta \rho_L = [1 + (C/X) + (1/x^2)]^{1/2}, C = 20$$

Single-phase pressure drop per unit length

$$\left(\frac{\Delta p}{\Delta L}\right)_L = \frac{f_L (G_L)^2}{2g_c D \rho_L}$$

Two-phase pressure drop per unit length

$$\left(\frac{\Delta p}{\Delta L}\right) = (\phi L)^2 \left(\frac{\Delta p}{\Delta L}\right)_L$$

The terms have their usual meaning.

7. A regenerator consists of 1.6 mm (0.063 in) diameter lead shot (density, 11,350 kg/m<sup>3</sup> = 708.6 lbm/ft<sup>3</sup>; specific heat, 0.1208 kJ/kg-K = 0.0288 Btu/lbm-°F). The porosity or void volume of the matrix is 0.38. The lead shot is contained inside a pipe having an ID of 154 mm (6.065 in) and a length of 915 mm (36.0 in). Nitrogen gas at an average pressure of 2 atm (202.6 kPa or 29.4 psia) and an average temperature of 200 K (360 °R) flows through the regenerator at a mass flow rate 0.080 kg/s (635 lbm/hr). Determine the convective heat transfer coefficient and the friction factor for the regenerator.

At 200K and 202.6 kPa, the following properties for nitrogen gas are found:

Viscosity,  $\mu = 12.95 \mu\text{Pa}\cdot\text{s} = 0.0313 \text{ lbm/ft}\cdot\text{hr}$

Specific heat,  $c_p = 1.043 \text{ kJ/kg}\cdot\text{K} = 0.2491 \text{ Btu/lbm}\cdot\text{°F}$

Prandtl number,  $Pr = 0.750$

Density,  $\rho = (1.711)(2) = 3.422 \text{ kg/m}^3 = 0.214 \text{ lbm/ft}^3$

The following equations may be used for calculations:-  
The mass flow rate per unit free flow area,

$$G = \frac{m}{e_v A_f r}$$

The equivalent diameter for the flow passage:

$$D_e = \frac{2e_v D_s}{3(1-e_v)}$$

The Colburn J-factor for packed spheres

$$J_H = 0.23 Re^{-0.3} = h_c Pr^{2/3} / C_p G$$

For  $Re < 1000$ ,

$$f = (172.6/Re) (1 + 0.0288 Re^{0.86})$$

The pressure drop through the regenerator matrix

or

The terms have their usual meaning.

8. Write short notes on any **four** of the following:

- a) Joule-Thomson expansion
- b) Gifford-McMohan Refrigerator
- c) Plate-fin Heat Exchanger
- d) Unique properties of Helium-4
- e) The Kapitza Process

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